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(54) **Process for forming a punch rivet connection**

Verfahren zur Formung einer Stanznietverbindung

Procédé pour la formation d'une connection par rivets poinçonnantes

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Description

[0001] The invention relates to a process for forming a punch rivet connection.

[0002] To form a punch rivet connection with which at least two parts to be joined can be connected to one another by a rivet, it is not necessary for the parts to be joined to be pre-punched. It is known that a punch rivet connection can be made using a solid rivet or hollow rivet.

[0003] A punch rivet connection is formed with a solid rivet by placing the parts to be joined on a die. A holding-down device is brought into contact with the parts to be joined above the die. The parts to be joined are clamped between the holding-down device and the die. The holding-down device is hollow in design. The rivet is arranged in it. A plunger acts on the rivet so that the plunger punches the rivet through the parts to be joined. The rivet punches a hole in the parts to be joined so the pre-punching required in conventional riveting processes is unnecessary. Once the rivet has penetrated the parts to be joined, the holding-down device presses the parts to be joined against the die which comprises a ferrule. The force of the holding-down device and the geometry of the die result in plastic deformation of the die-side part to be joined which flows partially into an annular groove in the punch rivet. The solid rivet is not deformed. The parts to be joined are reached by the geometry of the rivet head and by the die-side connection of the part to be joined to the rivet in the annular groove.

[0004] Hydraulically operated joining devices are used to form such a punch rivet connection. The plunger is actuated by a hydraulic cylinder unit. The cost of producing such joining devices is relatively high. In particular, process control for achieving high-quality punch rivet connections gives rise to problems. In particular, hydraulically operated joining devices are subject to variations in the force exerted by the plunger owing to changes of viscosity. The changes in the viscosity of the hydraulic medium are substantially dependent on temperature. A further drawback of hydraulically operated joining devices is that the hydraulic medium, which may be oil, has a hydropscopic effect so it is necessary to exchange the hydraulic fluid at predetermined time intervals.

[0005] When forming a punch connection with a hollow rivet - the same applies to a semi-hollow rivet - the hollow rivet penetrates the plunger-side part to be joined and penetrates partially into the die-side part to be joined. The die is so designed that the die-side part to be joined as well as the rivet are deformed to a closing head. An example of a design of a joining device for forming a punch rivet connection with a hollow rivet is known from DE 44 19 065 A1. Hydraulically operating joining devices are also used for producing a punch rivet connection with a hollow rivet.

[0006] Such a device and the related punch riveting process is known from document WO 94/14554 A.

[0007] The object of the present invention is to provide a process for forming a punch rivet connection by means of which the production costs for carrying out the process can be reduced. A further object of the invention is to monitor the formation of a punch rivet connection to improve quality assurance.

[0008] This object is achieved according to the invention by a process having the features of Claim 1.

[0009] With the process according to the invention for forming a punch rivet connection, it is proposed that a plunger and optionally a holding-down device be driven via a transmission unit which converts a rotational movement of a drive unit into a translation movement of the plunger or of the holding-down device. The relatively high production costs incurred with known processes when the plunger and optionally a holding-down device is or are hydraulically operated are avoided when carrying out the process. A further advantage of the process is that relatively good control of the process can be achieved by converting the rotational movement of a drive unit into a translation movement of the plunger, as an electric motor can be used as drive unit. Different plunger speeds can also be achieved with the process control according to the invention. A further advantage of the process is that process control is independent of external influences. For example, whereas the ambient temperature is involved in hydraulic actuation of the plunger as it affects the hydraulic medium, this influence is absent from the process according to the invention.

[0010] According to a further advantageous embodiment of the process, it is proposed that the speed of the drive unit be variable. Owing to this feature, the speed with which the plunger or the holding-down device acts on the parts to be joined or the rivet can be varied. The speed of the drive unit can be adjusted as a function of the properties of the rivet and/or the properties of the parts to be joined. The advantage of the adjustable speed of the drive unit also resides in the fact that, for example, the plunger and optionally the holding-down device is initially moved at high speed to rest on the parts to be joined and the plunger and optionally the holding-down device is then moved at a lower speed. This has the advantage of allowing relatively fast positioning of the plunger and the holding-down device. This also affects the cycle times of a joining device.

[0011] According to a further advantageous idea, it is proposed that the plunger and optionally the holding-down device be movable from a predeterminable rest position. The rest position of the plunger and optionally of the holding-down device is selected as a function of the design of the parts to be joined. If the parts to be joined are, for example, smooth metal plates, the distance between a riveting unit which comprises the plunger and the holding-down device and a die can be slightly greater than the thickness of the superimposed parts to be joined. If a part to be joined has a ridge, as viewed in the feed direction of the part to be joined, the rest position of the riveting unit is selected such that the

ridge can be guided between the riveting unit and the die. Therefore, it is not necessary for the riveting unit always to be moved into its maximum possible end position which is defined by maximum spacing between the riveting unit and a die.

[0012] According to a further advantageous embodiment of the process, it is proposed that the process data be determined during a punch riveting procedure.

[0013] In particular, the travel of the plunger and optionally of the holding-down device is determined during a punch riveting procedure. The travel of the plunger and optionally of the holding-down device is determined particularly easily as the stroke of the plunger or holding-down device can be determined from the number of rotations of the drive unit on the basis of the known transmission ratios from the rotational movement of the drive unit into a translation movement of the plunger or the holding-down device. For this purpose, the drive unit can be provided with known aids, for example an incremental disc. It is also possible to use a stepping motor as drive unit.

[0014] The force of the plunger and optionally of the holding-down device on the parts to be joined is preferably determined during a punch riveting procedure. A quality statement about the punch rivet connection can be derived from the trend of the force during the joining procedure, as described hereinafter.

[0015] According to a further advantageous idea, it is proposed that the power consumption of the drive unit be determined during a punch riveting procedure. The power consumption of the drive unit is substantially proportional to the force of the plunger and optionally of the holding-down device on the parts to be joined, so the force can be determined directly. Additional gauges are not necessarily required to determine the force. The power consumption can be determined using simple components.

[0016] In addition to or as an alternative to the determination of the power consumption or of the force of the plunger, it is proposed that the torque of the drive unit and/or of the transmission unit be determined during a punch riveting procedure. The torque of the drive unit and/or of the transmission unit is also proportional to the force of the plunger and optionally of the holding-down device on the parts to be joined. A quality statement about the punch riveting procedure or about the punch rivet connection can also be obtained from the torque trend.

[0017] According to a further advantageous embodiment of the process, it is proposed that a force or a characteristic, corresponding to the force, of the plunger and optionally of the holding-down device be measured during a joining procedure as a function of the displacement of the plunger or of the plunger and the holding-down device. This measurement produces an actual trend. This actual trend is compared with a desired trend. If comparison shows that the determined actual trend deviates from the desired trend by a predetermined limit

value in at least one predetermined range, a signal is triggered. This process control has the advantage, in particular, that it permits qualitative monitoring of the formation of a punch connection.

[0018] According to a further advantageous embodiment of the process it is proposed that the actual trend be compared with the desired trend at least in a region in which clinching is substantially completed by the force of the plunger on a rivet which has come to rest on the parts to be joined and a rivet has penetrated into the plunger-side part to be joined. A statement as to whether a rivet has been supplied and the rivet has also been correctly supplied can be obtained by comparing the actual force/displacement trend with the desired trend. The term 'correctly supplied' means a supply where the rivet rests in the correct position on the part to be joined. It can also be determined from the result of this comparison whether, for example, an automatic supply of rivets is being provided correctly.

[0019] According to a further preferred embodiment of the process, the actual trend is compared with the desired trend at least in a region in which the parts to be joined have been substantially punched by the force of the plunger on a rivet, in particular a solid rivet, and the holding-down device exerts a force on the plunger-side part to be joined. This has the advantage that it is possible to check whether the rivet actually penetrated the parts to be joined.

[0020] According to a further advantageous embodiment of the process, it is proposed that the actual trend be compared with the desired trend at least in a region in which a rivet, in particular a hollow rivet, substantially penetrated the plunger-side part to be joined owing to the force of the plunger and a closing head was formed on the rivet. It is thus also possible to check whether the parts to be joined also have a predetermined thickness.

[0021] According to a further idea, a comparison between the actual trend and the desired trend is proposed at least in a region in which a closing head is substantially formed on the rivet, in particular a hollow rivet, and clinching of the rivet takes place. It is thus possible to check whether the rivet ends flush with the surface of the plunger-side part to be joined.

[0022] It is also proposed that a force of the plunger or of the plunger and the holding-down device on the parts to be joined or a characteristic corresponding to the force be determined from the power consumption. The trend of the force as a function of the displacement of the plunger or of the plunger and the holding-down device can be allocated to specific parameters such as a thickness of the parts to be joined, material of the parts to be joined, form and material of the punch rivet. Such a trend can be used for controlling a joining device if similar parts to be joined are to be connected to one another by comparable punch rivets. This has the advantage that the expenditure for determining the most desirable process parameters for forming a punch rivet can be reduced.

[0023] Further details and advantages of the process according to the invention and of the joining device are described with reference to a preferred embodiment of a joining device illustrated in the drawings.

[0024] Figure 1 is a schematic view of a joining device.

[0025] Figure 2 is a section through a joining device.

[0026] Figure 3 is a force/displacement graph of a punch riveting procedure with a solid rivet.

[0027] Figure 4 is a force/displacement graph of a punch riveting procedure with a hollow rivet.

[0028] Figure 1 is a schematic view of the design of a joining device for punch rivets. The joining device has an electric motor driven drive unit 1. The drive unit 1 is connected to a transmission unit 2. A drive shaft of the drive unit 1 can be coupled to the transmission unit 2. The coupling can preferably be releasable in design so different transmission units 2 can be used. The transmission unit 2 preferably has at least one gear. This is, in particular, a reduction gear. A gear which has at least one predetermined reduction ratio is preferred.

[0029] The transmission unit is connected to a plunger 4 or to the plunger 4 and the holding-down device 5. Whether merely the plunger 4 or also the holding-down device 5 is connected to the transmission unit 2 depends on whether the joining device is used to form a punch rivet connection with a solid rivet or a hollow rivet. If the joining device is used for forming a punch rivet connection by means of a solid rivet, the holding-down device 5 is also coupled to the transmission unit 2.

[0030] The plunger 4 or the plunger 4 and the holding-down device 5 are connected to the transmission unit 2 via a spindle drive 3. The spindle drive 3 can also be part of the transmission unit 2 so they form a constructional unit. The spindle drive 3 is preferably a circulating ball spindle drive.

[0031] The plunger 4 and the holding-down device 5 are movable in the direction of the arrow shown in Figure 1. A die 6 is arranged beneath the plunger 4. Two parts to be joined 7, 8 are arranged schematically on the die 6.

[0032] The joining device also comprises a control unit 9 for controlling the drive unit 1. A monitoring unit 10 which comprises at least one sensor for detecting process data is connected to the control unit 9. A connection between the monitoring unit and the drive unit 1, the transmission unit 2 and the spindle drive 3 is shown schematically in Figure 1. The drive unit 1, the monitoring unit 2 and the spindle drive 3 can have corresponding sensors for picking up specific characteristics, the output signals of which are processed in the monitoring unit 10. The monitoring unit 10 can be part of the control unit 9, the monitoring unit 10 emitting input signals as open and closed loop control variables to the control unit 9. The sensors can be displacement and force transducers which determine the displacement of the plunger 4 and the force of the plunger 4 on the parts to be joined 7, 8. A sensor which measures the power consumption of the electric motor action drive unit 1 can also be provided.

[0033] A punch rivet is arranged within the holding-down device to form a punch rivet connection between the parts to be joined 7, 8. The plunger 4 is displaceable relative to the holding-down device 5. The plunger 4 exerts a force on a punch rivet by means of which the punch rivet connection is obtained. The drive unit 1 is set into operation for this purpose. The rotational movement of the drive unit 1 is converted via a transmission unit 2 and, in the embodiment illustrated, the spindle drive 3 into a translation movement of the plunger 4 and the holding-down device 5.

[0034] Figure 2 is a partial section through a joining device. The joining device has an electric motor operated drive unit 1. The drive unit 1 is connected to the transmission unit 2. The transmission unit 2 is arranged in an upper end region of a housing 25. The housing 25 is connected to a framework 24.

[0035] The drive shaft 11 of the drive unit 1 is connected to a belt wheel 12 of the transmission unit 2. The belt wheel 12 drives a belt wheel 14 via an endless belt 13 which may be a flexible toothed belt. The diameter of the belt wheel 12 is substantially smaller than the diameter of the belt wheel 14, allowing a reduction in the speed of drive shaft 11. The belt wheel 14 is rotatably connected to a drive bush 15. A gear with gear wheels can also be used instead of a transmission unit 2 with belt drive. Other alternatives are also possible. A rod 17a is transversely displaceable within the drive bush 15 which is appropriately mounted. The translation movement of the rod 17a is achieved via a spindle drive 3 having a spindle nut 16 which cooperates with the rod 17a. At the end region of the rod 17a remote from the transmission unit 2 there is formed a guide member 18 into which the rod 17a can be introduced. A rod 17b adjoins the rod 17a. An insert 23 is provided in the transition region between the rod 17a and the rod 17b. The insert 23 has pins 20 which project substantially perpendicularly to the axial direction of the rod 17a or 17b and engage in slots 19 in the guide member 18. This ensures that the rod 17a and 17b does not rotate. The rod 17b is connected to a plunger 4. The plunger 4 is releasably arranged on the rod 17b so it can be formed according to the rivets used. A stop member 22 is provided at the front end region of the rod 17b. Spring elements 21 are arranged between the stop member 22 and the insert 23. The spring elements 21 are spring washers. The spring elements 21 are arranged in a tubular portion of the guide member 18. The guide member 18 is arranged so as to slide in the housing 25. Figure 2 shows the joining device in a position in which the plunger 4 and the holding-down device 5 rest on the parts to be joined 7, 8, the parts to be joined 7, 8 resting on the die 6.

[0036] In a punch rivet connection formed by a grooved solid rivet, the rivet is pressed through the parts to be joined 7, 8 by the plunger 4 once the parts to be joined 7, 8 have been fixed between the die 6 and the holding down device 5. The rivet punches a hole in the parts to be joined 7, 8 during this procedure.

[0037] The holding-down device 5 and the plunger 4 effect clinching which extends to point A of the curve in the force/displacement graph shown in Figure 3. The rivet then punches a hole in the parts 7, 8 to be joined, this procedure taking place in the portion A - B. After punching has taken place, the holding-down device presses against the parts to be joined 7, 8. The holding-down device presses against the die such that the die-side part to be joined 8 flows into the groove of the rivet owing to a corresponding design of the die 6. This portion of the process lies between points B - C.

[0038] Regions in which the actual trend of the force or a characteristic corresponding to the force as a function of the displacement can be compared with a desired trend are designated by V1, V2 and V3 in Figure 3. The regions V1, V2 and V3 are significant for the quality of the punch rivet connection. However, the entire actual trend can also be compared with the desired trend instead of selected regions V1, V2 or V3. A statement as to whether, for example, a solid rivet is arranged on the plunger-side part to be joined 7 with the correct orientation can be obtained by comparison in the region V1. A statement about the clinch behaviour of the parts to be joined can also be derived. If the clinch behaviour differs, it can be concluded that, for example, the plunger-side part to be joined consists of an incorrect material.

[0039] A statement as to whether, for example, complete punching of the parts to be joined 7, 8 has occurred can be obtained by comparison in region V2.

[0040] Comparison between the actual trend and the desired trend in region V3 provides a statement as to whether the material of the die-side part to be joined 8 has flown into an annular groove in a rivet, not shown.

[0041] The trend of the force as a function of the displacement can be determined by the process according to the invention from the power consumption of the electric motor drive 1.

[0042] Figure 4 is a schematic view of a force/displacement graph of the type produced during a punch riveting procedure using a hollow rivet. The force/displacement graph shows that essentially four process portions can be detected in the punch rivet procedure using a hollow rivet. A first process portion which essentially corresponds to a clinching procedure can be seen up to point A. A second process portion which essentially corresponds to the cutting procedure can be seen between points A and D. During the cutting process, the plunger 4 and therefore also a rivet covers a relatively great displacement s, the force exerted by the plunger 4 on the rivet being relatively constant.

[0043] Once the rivet has cut through the plunger-side part to be joined 7, the rivet is spread in the die 6 as the force of the plunger 4 increases. This portion of the process is located between points D - E of the force/displacement graph according to Figure 4. The die-side part to be joined 8 is deformed by the die 6 during this procedure.

[0044] If the force exerted on the rivet by the plunger

4 is sustained, the rivet is compressed. The compression process is shown in portion E - F in Figure 4. If the head of the punch rivet lies in the plane of the plunger-side part to be joined 7, the punch rivet connection is produced.

[0045] The force/displacement trend can be determined from the process data. With a known force/displacement trend which serves as a reference trend, the quality of a punch connection can be determined by means of the actual trend of the force as a function of the displacement.

[0046] Figure 4 shows regions H1 - H4 in which the actual trend of the force as a function of the displacement is checked with a desired trend. The regions H1 - H4 are selected at the significant transition points of the process steps, as described hereinbefore. A quality statement about the punch rivet connection can therefore be obtained. The entire actual trend can also be checked with a desired trend rather than individual regions H1 - H4, the desired trend forming a band within whose limits the actual trend is to lie.

Claims

1. Process for forming a punch rivet connection in which a plunger (4) and a holding-down device (5) are driven by a transmission unit (2) which converts a rotational movement of an electrically powered drive unit (1) into a translation movement of the plunger (4) and/or of the holding-down device (5).
2. Process according to claim 1, in which the speed of the drive unit (1) is variable.
3. Process according to claim 1 or claim 2, in which the plunger (4) and/or the holding-down device (5) are initially moved at high speed so as to rest on the parts to be joined and the plunger (4) and/or the holding-down device (5) then optionally moved at a lower speed.
4. Process according to one of claims 1 to 3, during which the plunger (4) and/or the holding-down device (5) can be moved from a predeterminable rest position.
5. Process according to one of claims 1 to 4, in which the process data are determined during a punch riveting procedure.
6. Process according to one of claims 1 to 5, in which a displacement of the plunger (4) and/or the holding-down device (5) is determined during a punch riveting procedure.
7. Process according to one of claims 1 to 6, in which a force exerted by the plunger (4) and/or the hold-

ing-down device (5) is determined on parts to be joined (7, 8) during a punch riveting process.

8. Process according to one of claims 1 to 7, in which the power consumption of the drive unit (1) is determined during a punch riveting process.

9. Process according to one of claims 1 to 8, in which a torque of the drive unit (1) and/or of the transmission unit (2) is determined during a punch riveting procedure.

10. Process according to one of claims 5 to 9, in which a force or a characteristic corresponding to the force of the plunger (4) and/or of the holding-down device (5) as a function of the displacement of the plunger (4) and/or the holding-down device (5) is measured during a joining procedure and an actual trend determined and the actual trend compared with a desired trend and a signal triggered when the determined actual trend differs from the desired trend by a predetermined limit value in at least one predetermined region.

11. Process according to claim 10, in which a comparison between the actual trend and the desired trend takes place at least in a region (V1, H1) in which clinching effected on the parts to be joined by the force of the plunger (4) acting on a rivet essentially takes place and a rivet penetrates into the plunger-side part to be joined (7).

12. Process according to claim 10 or 11, in which the actual trend is compared with the desired trend at least in a region (V2) in which punching of the parts to be joined (7, 8) is essentially effected by the force of the plunger (4) acting on a rivet, in particular a solid rivet, and the holding-down device (5) exerts a force on the plunger-side part to be joined (7).

13. Process according to claim 10 or 11, in which the actual trend is compared with the desired trend at least in a region (H2) in which a rivet, in particular a hollow rivet, penetrates the plunger-side part to be joined (7) owing to the force of the plunger (4) and a closing head is formed on the rivet.

14. Process according to claim 10 or 11 or 13, in which the actual trend is compared with the desired trend at least in a region (H3) in which a closing head is essentially formed on a rivet, in particular a hollow rivet, and the rivet is compressed.

Patentansprüche

1. Verfahren zum Formen einer Stanznietverbindung, bei dem ein Stempel (4) und eine Niederhaltevor-

richtung (5) durch eine Kraftübertragungseinheit (2) angetrieben wird, die die Drehbewegung einer elektrisch gespeisten Antriebseinheit (1) in eine Translationsbewegung des Stempels (4) und/oder der Niederhaltevorrichtung (5) umwandelt.

2. Verfahren nach Anspruch 1, bei dem die Geschwindigkeit der Antriebseinheit (1) veränderlich ist.

3. Verfahren nach Anspruch 1 oder Anspruch 2, bei dem der Stempel (4) und/oder die Niederhaltevorrichtung (5) anfänglich mit hoher Geschwindigkeit bewegt werden, bis sie auf den zusammenzufügenden Teilen aufsitzen, und daß anschließend der Stempel (4) und/oder die Niederhaltevorrichtung (5) wahlweise mit einer geringeren Geschwindigkeit bewegt werden.

4. Verfahren nach einem der Ansprüche 1 bis 3, bei dessen Durchführung der Stempel (4) und/oder die Niederhaltevorrichtung (5) von einer vorbestimmbaren Ruheposition aus bewegt werden können.

5. Verfahren nach einem der Ansprüche 1 bis 4, bei dem die Verfahrensdaten während einer Stanzvernietungsprozedur bestimmt werden.

6. Verfahren nach einem der Ansprüche 1 bis 5, bei dem die Verschiebung des Stempels (4) und/oder der Niederhaltevorrichtung (5) während einer Stanzvernietungsprozedur bestimmt wird.

7. Verfahren nach einem der Ansprüche 1 bis 6, bei dem die auf den Stempel (4) und/oder die Niederhaltevorrichtung (5) ausgeübte Kraft auf die zusammenzufügenden Teile (7, 8) während des Stanzvernietungsprozesses bestimmt wird.

8. Verfahren nach einem der Ansprüche 1 bis 7, bei dem der Energieverbrauch der Antriebseinheit (1) während des Stanzvernietungsprozesses bestimmt wird.

9. Verfahren nach einem der Ansprüche 1 bis 8, bei dem das Drehmoment der Antriebseinheit (1) und/oder der Kraftübertragungseinheit (2) während einer Stanzvernietungsprozedur bestimmt wird.

10. Verfahren nach einem der Ansprüche 5 bis 9, bei dem eine Kraft oder eine Charakteristik entsprechend der Kraft des Stempels (4) und/oder der Niederhaltevorrichtung (5) als Funktion der Verschiebung des Stempels (4) und/oder der Niederhaltevorrichtung (5) während der Verbindungsprozedur gemessen und eine tatsächliche Tendenz bestimmt wird, und die ermittelte tatsächliche Tendenz mit einer gewünschten Tendenz verglichen wird, und ein Signal ausgelöst wird, wenn die bestimmte tatsäch-

liche Tendenz sich von der gewünschten Tendenz um einen vorbestimmten Grenzwert in mindestens einem vorbestimmten Bereich unterscheidet.

11. Verfahren nach Anspruch 10, bei dem der Vergleich zwischen der tatsächlichen Tendenz und der gewünschten Tendenz mindestens in einem Bereich (V1, H1) stattfindet, in welchem das Klinschen auf den zusammenzufügenden Teilen im wesentlichen durch die Kraft des auf den Niet einwirkenden Stempels (4) stattfindet, und der Niet in das anzufügende, stempelseitige Teil (7) eindringt. 5
12. Verfahren nach Anspruch 10 oder 11, bei dem die tatsächliche Tendenz mit der gewünschten Tendenz zumindest in einem Bereich (V2) verglichen wird, in welchem das Stanzen der zusammenzufügenden Teile (7, 8) im wesentlichen durch die Kraft des auf den Niet, insbesondere einen massiven Niet, des Stempels (4) bewirkt wird, und die Niederhaltevorrichtung (5) eine Kraft auf das anzufügende, stempelseitige Teil (7) ausübt. 10
13. Verfahren nach Anspruch 10 oder 11, bei dem die tatsächliche Tendenz mit der gewünschten Tendenz zumindest in einem Bereich (H2) verglichen wird, in welchem der Niet, insbesondere ein Hohl-niet, in das anzufügende, stempelseitige Teil (7) aufgrund der Kraft des Stempels (4) eindringt und ein Schließkopf auf dem Niet geformt wird. 15
14. Verfahren nach Anspruch 10 oder 11 oder 13, bei dem die tatsächliche Tendenz mit der gewünschten Tendenz zumindest in einem Bereich (H3) verglichen wird, in welchem der Schließkopf im wesentlichen auf dem Niet, insbesondere einem Hohl-niet, geformt wird und der Niet zusammengedrückt wird. 20

Revendications

1. Procédé pour former une connexion par rivet poinçonnant dans lequel un piston (4) et un dispositif de maintien (5) sont entraînés par une unité de transmission (2) qui convertit un mouvement rotatif d'une unité d'entraînement actionnée électriquement (1) en un mouvement de translation du piston (4) et/ou du dispositif de maintien (5). 25
2. Procédé selon la revendication 1, dans lequel la vitesse de l'unité d'entraînement (1) est variable. 30
3. Procédé selon la revendication 1 ou 2, dans lequel le piston (4) et/ou le dispositif de maintien (5) sont déplacés initialement à vitesse élevée pour venir en appui sur les pièces ou parties à relier et dans lequel le piston (4) et/ou le dispositif de maintien (5) sont déplacés ensuite facultativement à une vitesse plus 35

basse.

4. Procédé selon l'une quelconque des revendications 1 à 3, lors duquel le piston (4) et/ou le dispositif de maintien (5) peuvent être déplacés à partir d'une position d'appui pouvant être prédéterminée. 40
5. Procédé selon l'une quelconque des revendications 1 à 4, dans lequel les données de procédé sont déterminées lors d'un processus de rivetage par poinçonnement. 45
6. Procédé selon l'une quelconque des revendications 1 à 5, dans lequel un déplacement du piston (4) et/ou du dispositif de maintien (5) est déterminé lors d'un processus de rivetage par poinçonnement. 50
7. Procédé selon l'une quelconque des revendications 1 à 6, dans lequel une force exercée par le piston (4) et/ou le dispositif de maintien (5) est déterminée sur des parties à relier (7, 8) lors d'un procédé de rivetage par poinçonnement. 55
8. Procédé selon l'une quelconque des revendications 1 à 7, dans lequel la consommation d'énergie de l'unité d'entraînement (1) est déterminée lors d'un processus de rivetage par poinçonnement. 60
9. Procédé selon l'une quelconque des revendications 1 à 8, dans lequel un couple de l'unité d'entraînement (1) et/ou de l'unité de transmission (2) est déterminé lors d'un processus de rivetage par poinçonnement. 65
10. Procédé selon l'une quelconque des revendications 5 à 9, dans lequel une force ou une caractéristique correspondant à la force du piston (4) et/ou du dispositif de maintien (5) en fonction du déplacement du piston (4) et/ou du dispositif de maintien (5) est mesurée lors d'un processus de liaison et une tendance réelle est déterminée, et la tendance réelle est comparée avec une tendance voulue, et un signal est déclenché lorsque la tendance réelle déterminée diffère de la tendance voulue d'une valeur limite prédéterminée dans au moins une zone prédéterminée. 70
11. Procédé selon la revendication 10, dans lequel une comparaison entre la tendance réelle et la tendance voulue a lieu au moins dans une zone (V1, H1) dans laquelle le rivetage effectué sur les parties à relier par la force du piston (4) agissant sur un rivet a essentiellement lieu, et un rivet pénètre dans la partie à relier située côté piston (7). 75
12. Procédé selon la revendication 10 ou 11, dans lequel la tendance réelle est comparée à la tendance voulue au moins dans une zone (V2) dans laquelle 80

le poinçonnement des parties à relier (7, 8) est essentiellement effectué par la force du piston (4) agissant sur un rivet, en particulier un rivet plein, et le dispositif de maintien (5) exerce une force sur la partie à relier située côté piston (7).

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13. Procédé selon la revendication 10 ou 11, dans lequel la tendance réelle est comparée à la tendance voulue au moins dans une zone (H2) dans laquelle un rivet, en particulier un rivet creux, pénètre la partie à relier située côté piston (7) du fait de la force du piston (4) et une tête de fermeture est formée sur le rivet.

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14. Procédé selon la revendication 10 ou 11 ou 13, dans lequel la tendance réelle est comparée à la tendance voulue au moins dans une zone (H3) dans laquelle une tête de fermeture est formée essentiellement sur un rivet, en particulier un rivet creux, et le rivet est comprimé.

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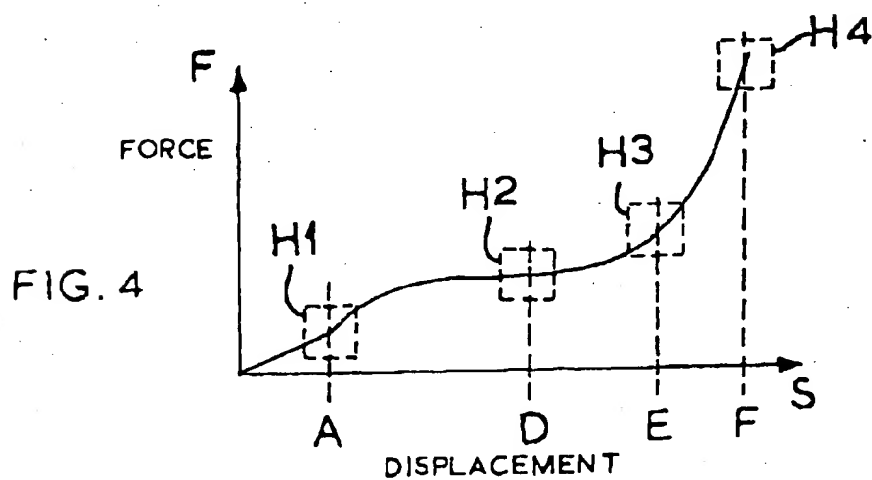
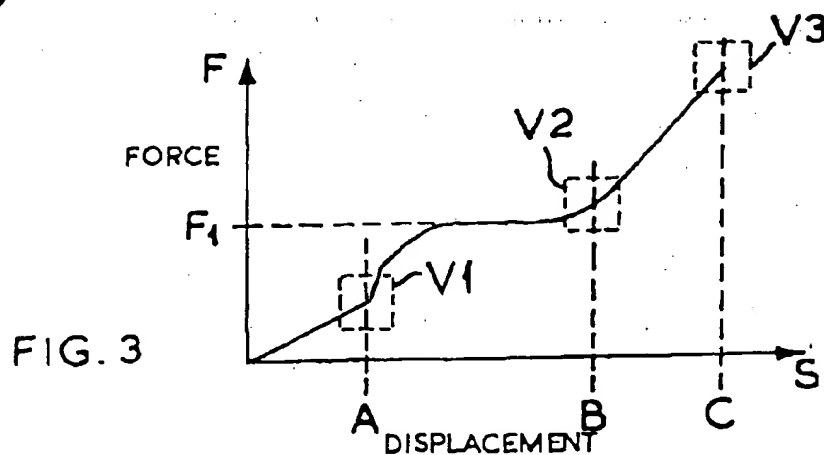
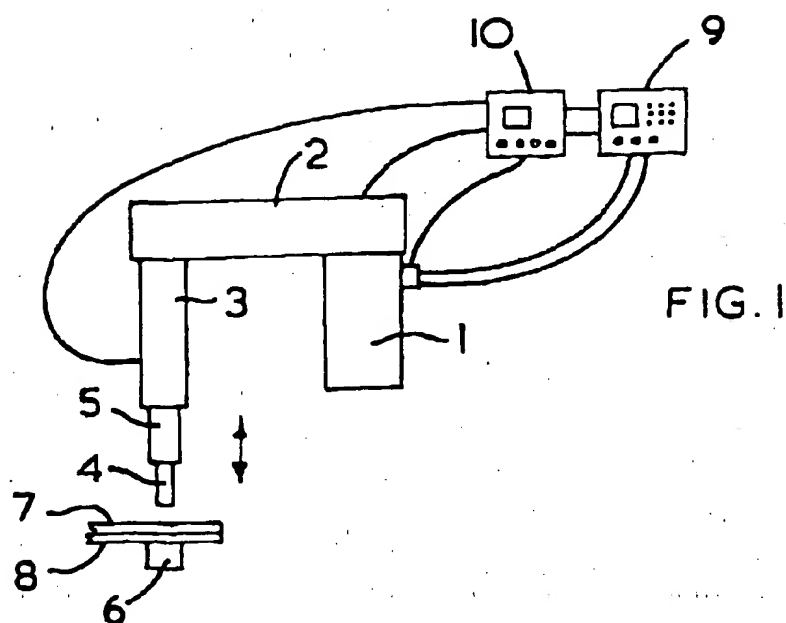
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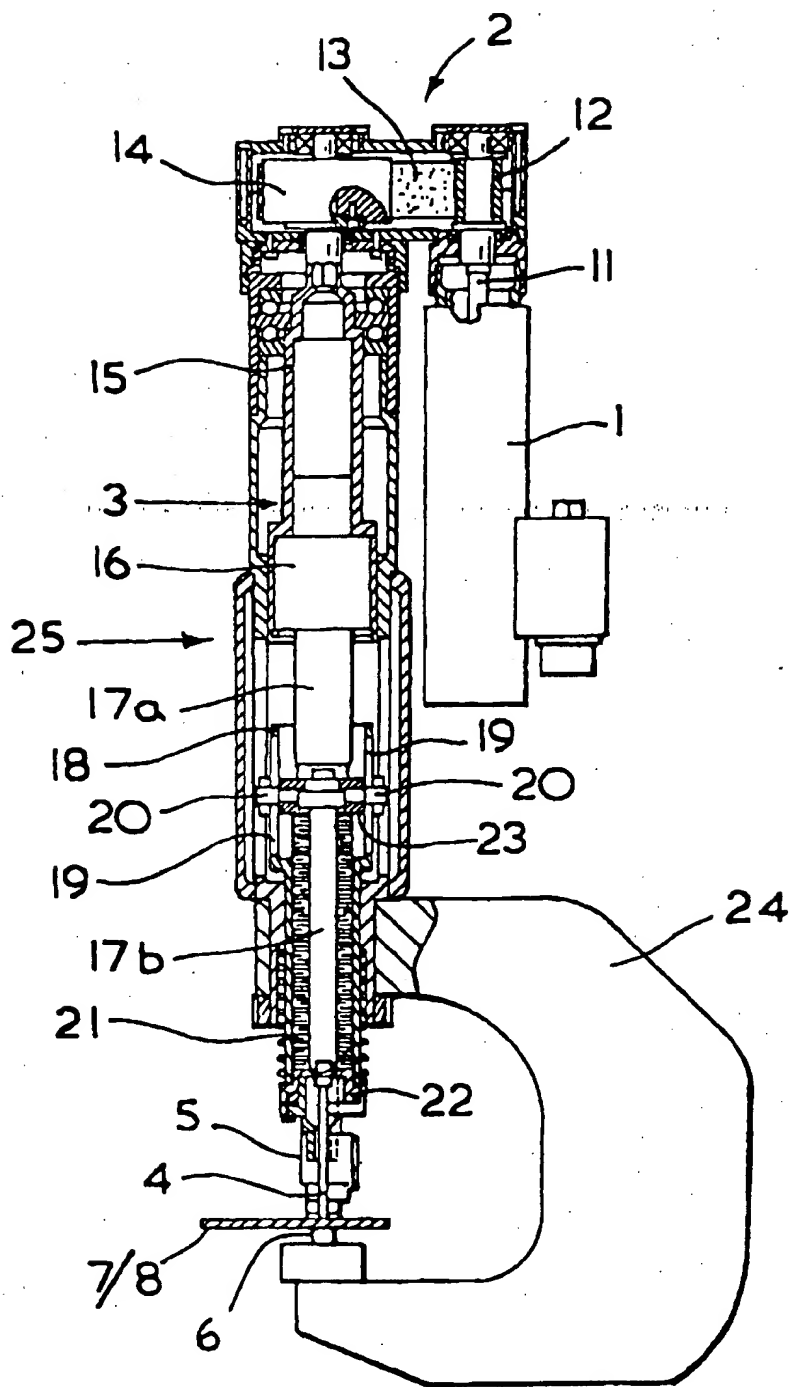


FIG. 2